

A handwritten signature in black ink, consisting of stylized, cursive letters.

**01.04.14 –**

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**- 2010**

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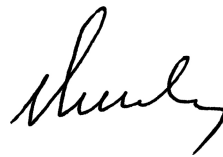
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2010 .

212.285.02, . - . .,



..

$$(Kn)$$
$$(Kn \rightarrow \infty)$$

[1]

(

GASMEMS)

[2].

[3]

[4].

[5, 6].

$$He \quad W \quad ( \quad )$$

2.2.2.2/5579

“(2009-

2010 )” CRDF ( REC RUXO-005-EK-06/  
BG4M05).

6. ;  
.
1. , : - ,  
*SiC* ,  
;  
 ,  
 ;  
2. ;  
 -  
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3. ;  
4. ( ) ,  
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5. , .  
1. :  
( - )  
( =0) ( =1)  
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2. : ,  
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3. , - ,  
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7. XIII « - » 5 - 9 2009,

8. 2<sup>nd</sup> GASMEMS Workshop – July 2010, Les Embiez, France;

9. 27th International Symposium on Rarefied Gas Dynamics (RGD27) July 10-15 2010, Pacific Grove, California, USA.

3 13 , .

103 105 , 5 , 44 , 8 .

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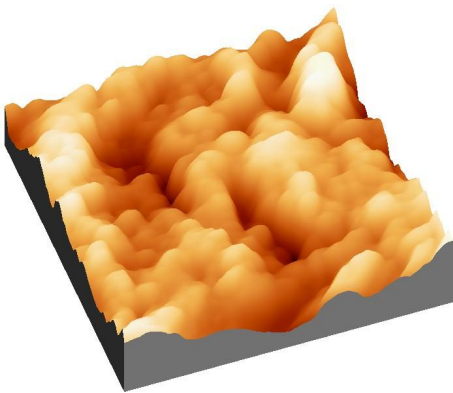
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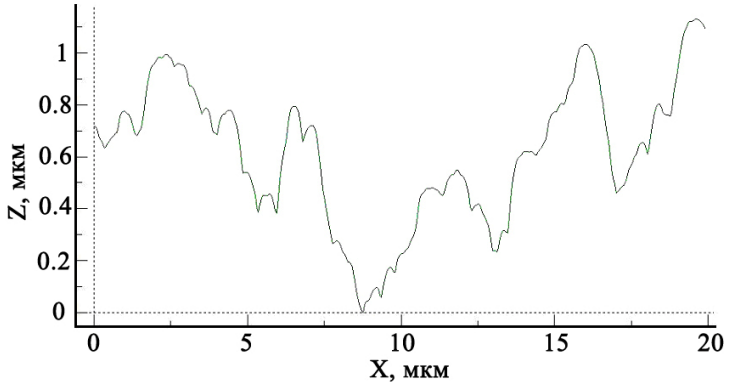
( ) SiC.

$$\{x_i, y_i, z_i\},$$

. 1. . 2



. 1. SiC 20×20



. 2. SiC

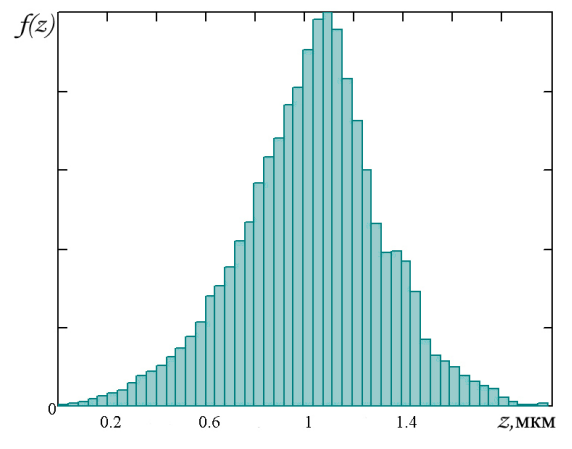


3).

[8],

1.

$D_f$ .

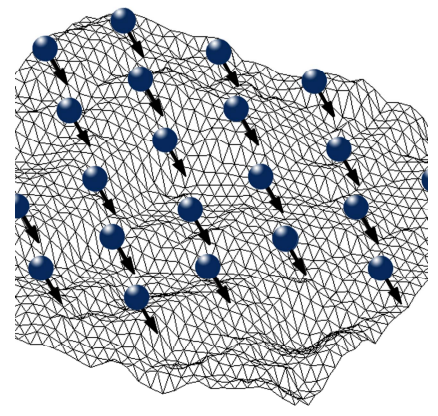


.3.

SiC

1. $\langle Z \rangle$ ,	$\sigma$ ,	$D_f$
1.106	0.275	2.46

. 4.

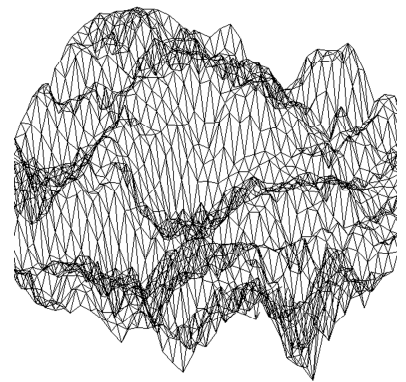
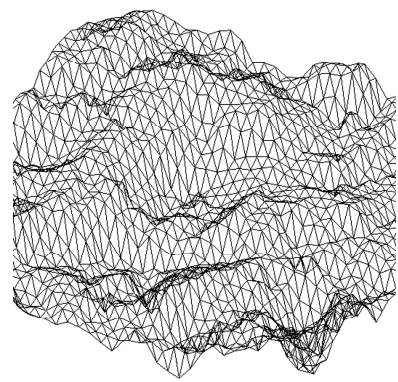
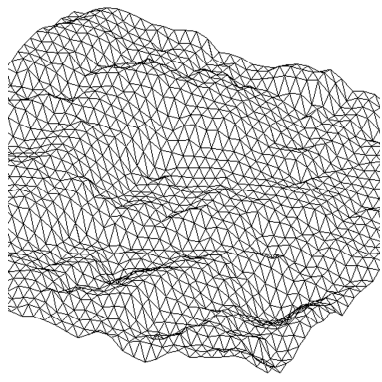


$H=0 \div 5.$   $=0$   
 $=5$   $z-$   
 $5$

$H = 1$

.4.

( . . 5).



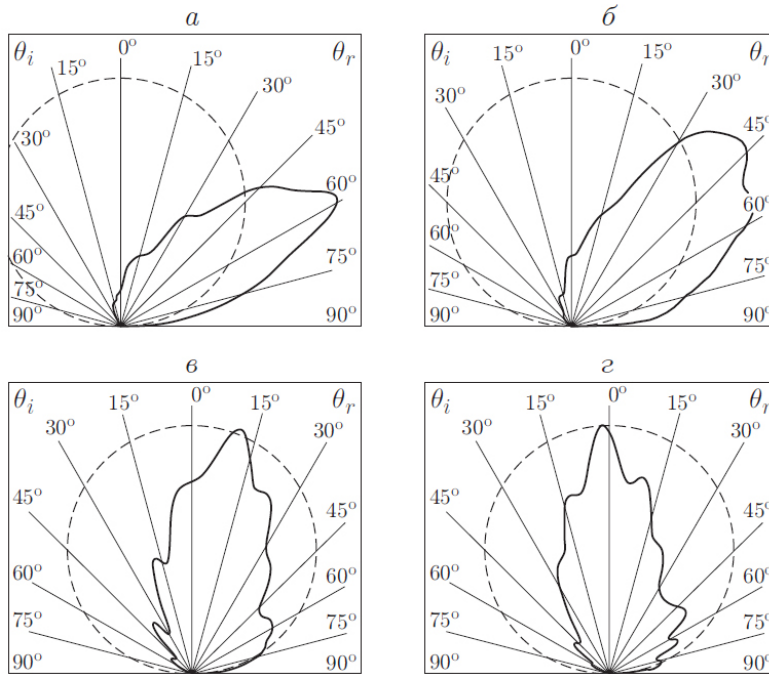
.5.

: -  $H=1$ , -  $H=3$ , -  $H=5$

( $\varepsilon = 0$ ).

$H = 1, 2, 3, 4, 5$   
 . 6.

$\theta_i = 75, 45, 15, 0$  .



. 6. ( $\varepsilon = 0$ )  
 $-\theta_i = 75, -\theta_i = 45, -\theta_i = 15, -\theta_i = 0$  ;

$H=1$  :  
 $\theta_i$

( $H=1$ )  
 $\begin{matrix} =1 & =5 \\ =1 & =2 \end{matrix}$

( $\varepsilon=1$ )

$\theta_i = 75, 45, 15, 0$

$H=1, 3, 5$ .

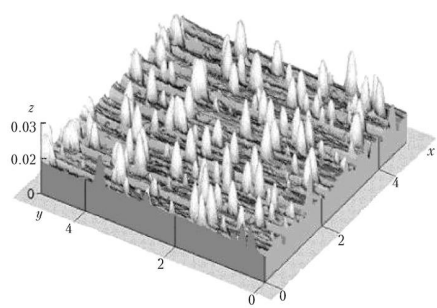
. 7

$v_y$ ,

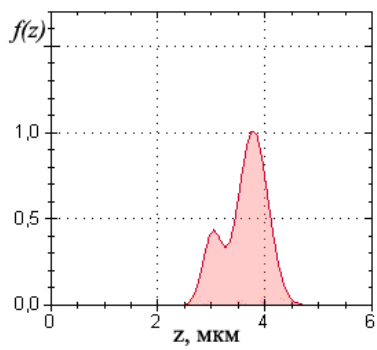
$H=3$ .

c  $v_y$  - . 7

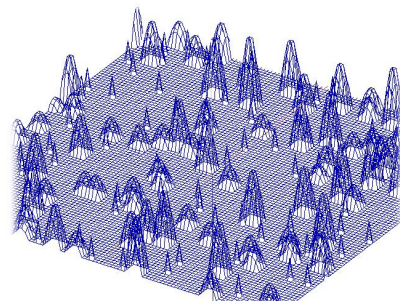




8.  $Si$   
( $5 \times 5$ )

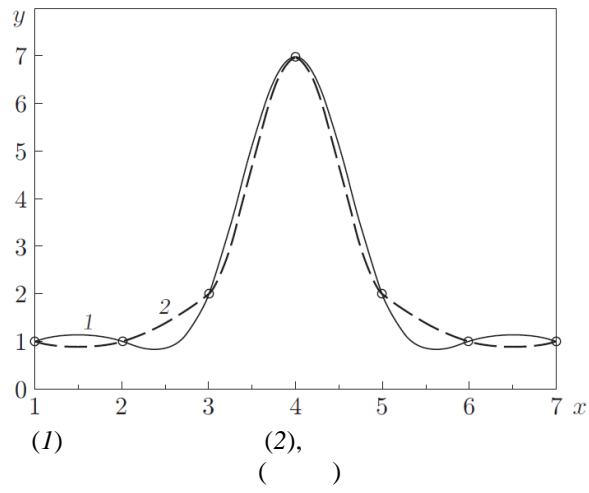


9.



10.

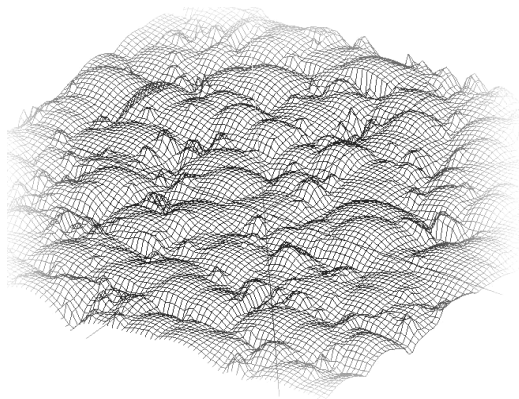
. 11.



“ ” (2) ,

$$z_{res} = \begin{cases} sum(z_1, z_2) \\ sub(z_1, z_2) \\ max(z_1, z_2) \\ min(z_1, z_2) \end{cases} \quad (2)$$

. 12, . 3.



. 12. « »

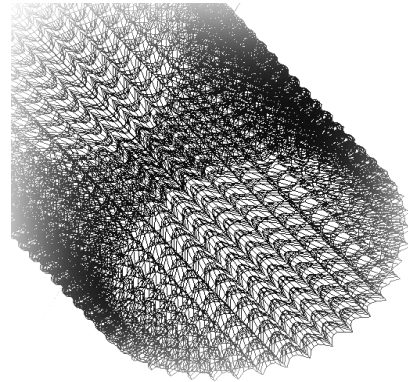
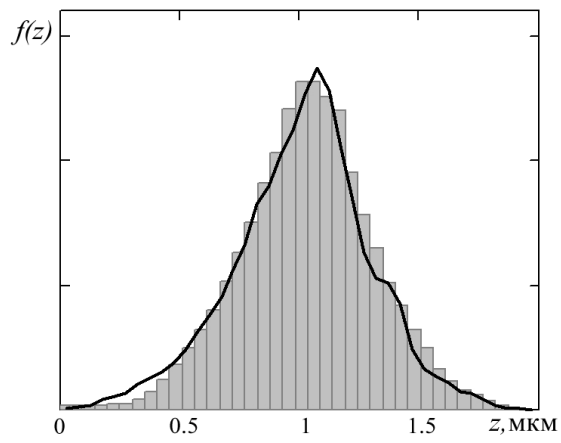
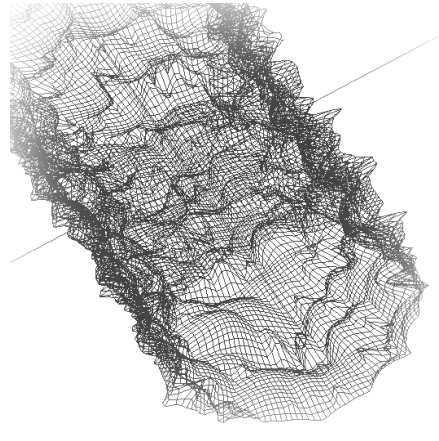
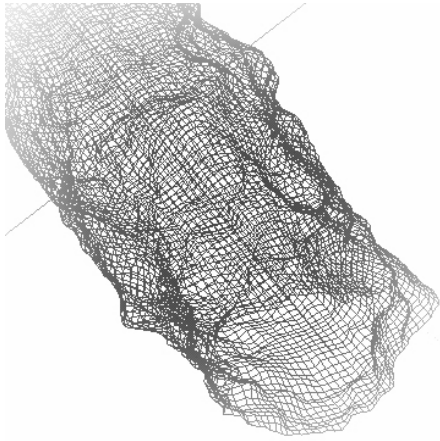
w.

[9].

$\varepsilon = 1$ .

( . . 13 ),  $w$  : 1 –  
 “ ” ( . . 5 ) ; 2 – ( . . 13 ),  
 ( . . 12) « »  
 ,  
 1 ( . . 13 ); 3 – ( . . 13 )  
 ( ) ,

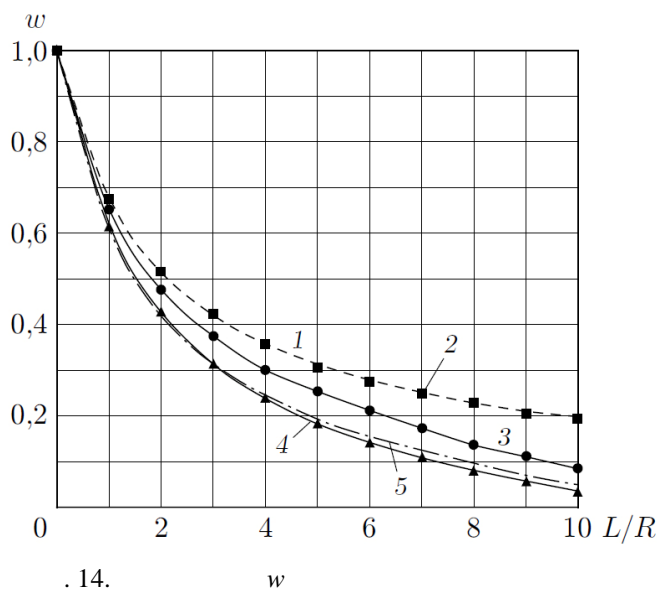
$$\dot{H}_{ave} = 1.1 \quad .$$



. 13. – , “ ” ( . . 12); – ( . . 5 ); –  
 : “ ” , “ ”  
 ; – “ ”

$w$ ,  $L$   
 $R$   
 [4] . 14.



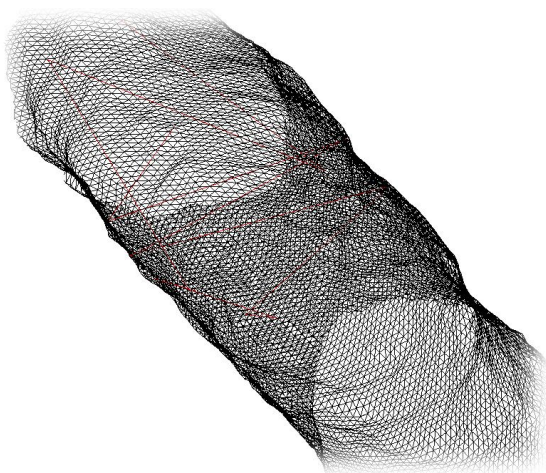


14.  $w$  : 1 - [4]; 2 - " " ( ; 3 - " ; 4 - " , " ; 5 - " ) ,

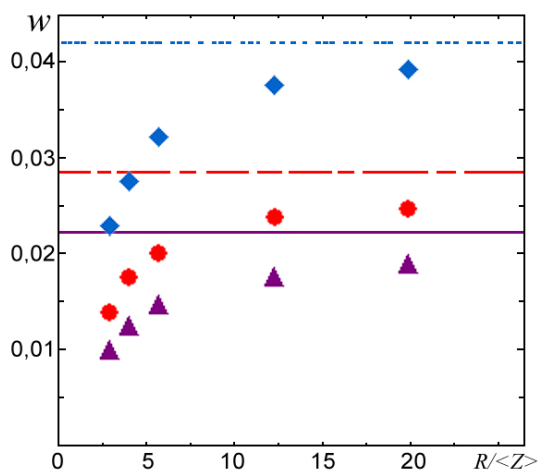
$L$   $R$   $w$   
 $\langle Z \rangle$   
 $\{ z_i \}$   $L/R = 60, 90 \quad 120.$   
 $H = 0 \div 1.$   $R/\langle Z \rangle = 5$   
 $(\varepsilon=1)$

15. [4]

16.



15.  $R/\langle Z \rangle = 5$

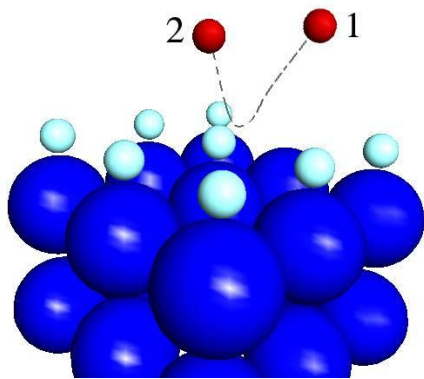


16.  $w$   
 $R/\langle Z \rangle$  :  $\diamond$ ,  $\bullet$ ,  $\blacktriangle$  -  $L/R=60, 90 \quad 120$   
[4]

15-20%

$$R/\langle Z \rangle.$$

5.1



. 17.

$He_{Wc}$

$\theta \sim 0.8$ ; 1, 2 –

$He$

$E_i$  –  
 $E_r$  –

$$\alpha = \frac{E_i - E_r}{E_i - E_s}, \quad (3)$$

( ),

,  $E_s$  –

: )

,

$W$

–

$T_s$ ; )

( )

; )

$T_g$ ;

)

$He$

; )

,

–

[11]; )

$E_i < 0,1$  ,

–

; )

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,

.



[10]

( )

,

$10^{-6}$

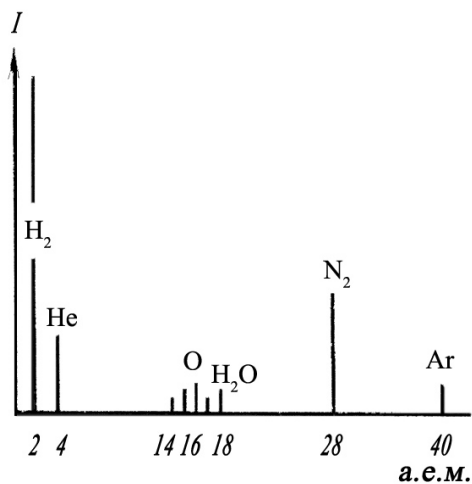
$10^{-10}$

*in situ*

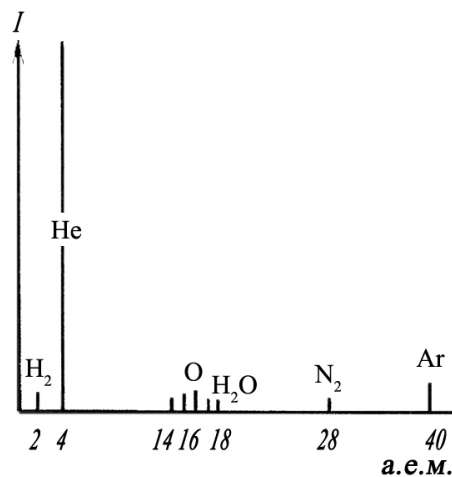
[12, 13].

*He - W*

. 18-20.



. 18.



. 19.

[10]

[10]

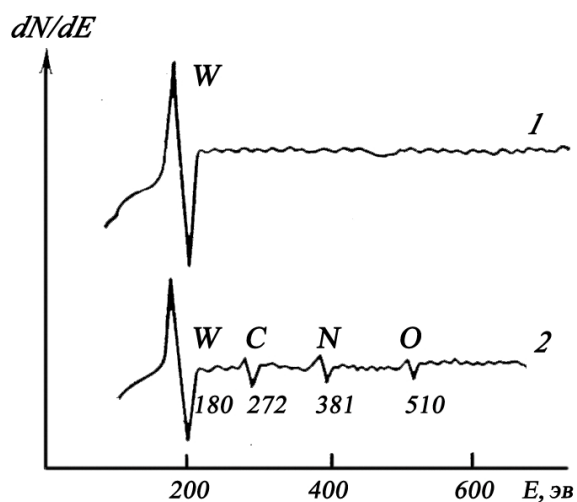
. 18 19

$CO_2$

$H_2O$ .

$H_2, He, N_2, Ar,$

$O_2,$



. 20.

[10]:

$I -$

2700 K, 2 -

$C, N, O -$

[14],

[7],

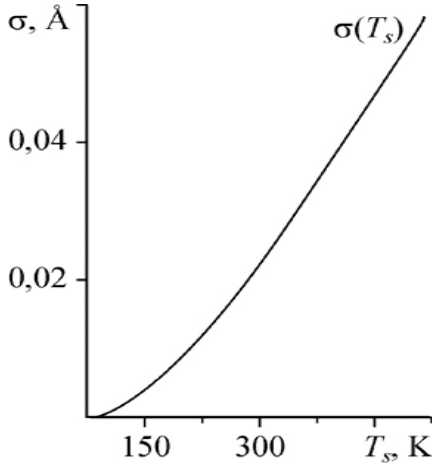
0.1Å.

<

,  $T_s$ ,  $T_s$ ,  $\sigma(T_s)$ ,

$$\sigma(T_s) = -4 \cdot 10^{-10} T_s^3 + 5 \cdot 10^{-7} T_s^2 - 4 \cdot 10^{-5} T_s. \quad (4)$$

. 21.



. 21.

$\sigma(T_s)$   $W$

$R(\tau)$  -

$\tau$ .

$$\mathbf{R}(\tau) = \mathbf{R}(0) + \dot{\mathbf{R}}(0)\tau - (1/M_g) \sum_{\mathbf{M}} \int_0^\tau ds \int_0^s du \mathbf{F}_{gs,ga}(\mathbf{M}, u). \quad (5)$$

$\mathbf{N}$ -

$M_s$

:

$$\mathbf{Y}(\mathbf{N}, \tau) = \mathbf{Y}_t(\mathbf{N}, \tau) + (1/M_s) \left[ \sum_{\mathbf{M}} \int_0^\tau ds \int_0^s du \mathbf{F}_{ss,sa}(\mathbf{M}, u) + \int_0^\tau ds \int_0^s du \mathbf{F}_{gs}(\mathbf{N}, u) \right], \quad (6)$$

$He$

$W$

(

)

,

$W$

.22.

$k_W$ ,

, «

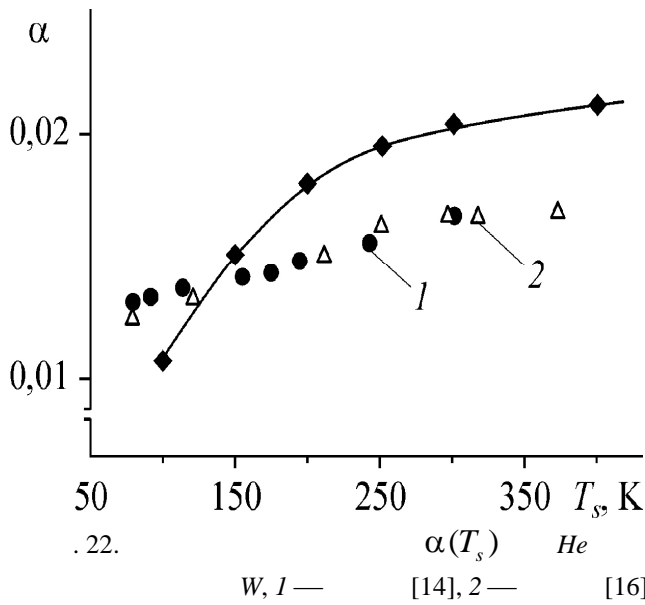
»

$W$

:

$$F_W(\Delta r) = -k_W \Delta r_W, \quad (7)$$

$\Delta r_W$  -



He

W,  
 $k_W$ ,  
 $k_W$

$\alpha$   
 [14, 16].

He

( ).

$T_s$

$k_a$

W=O.

$k_a$

$k_a$

$$F(\Delta b) = -k_a \Delta b = -k_a (b - b_0), \quad (8)$$

$b_0$  -

,  $b$  -  
 $k_a$

$T_s$ ,

$k_W$

W-W.

2

2.	$k_W$	$k_a$	W-W	W=O	$T_s$	$T_g$
	(1/Å)			$T_s$ (K)		$T_g$ (K)
$k_W$ W-W	500			150-450		150-450
$k_a$ W=O	30			298		300
	280			446		300

. 23

$\alpha$

[10],

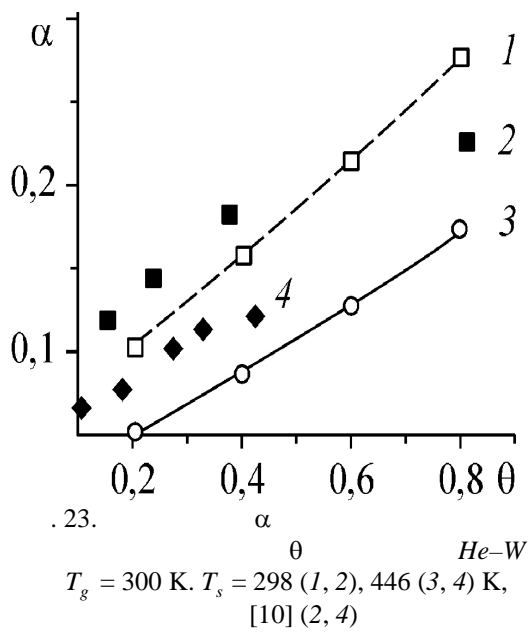
$\theta$

$T_s = 298$  446 K

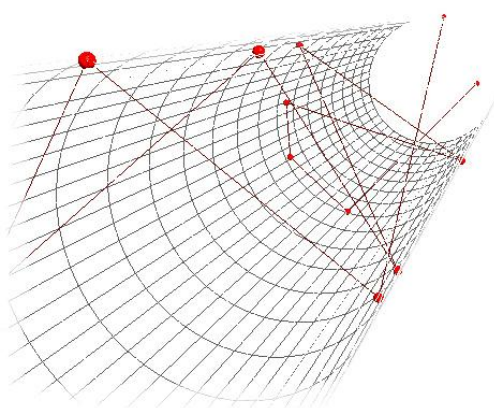
$T_g = 300$  K.

$k_a$  c

$T_s$



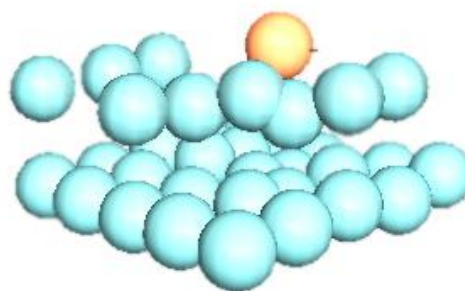
5.2



$k_O$ ,

( $\theta=0.5$ )

$C_m H_n$ ,  
 $T_s$   
 “ ” ,  
 $N_2$ ,  $O_2$ ,  $H_2O$ ,  
 $CO$ ,  $CO_2$ ,  $H_2O$ .  
 $W=O$ ,  
 2000 K.  
 $He$   $\alpha$   $\theta$



*Ar*

$k_W$ ,

$H_2O$ ,  $CO$ ,  $NO$ .



5.  $\frac{1}{2} \left( \frac{1}{2} + \frac{1}{2} \right) = \frac{1}{2}$  (100%)

1.  $\dots$ ,  $\dots$ ,  $\vdots$   $\dots$  //  $\dots$  2009.  $\dots$  50,  $\dots$  5.  
с. 20-27.

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